

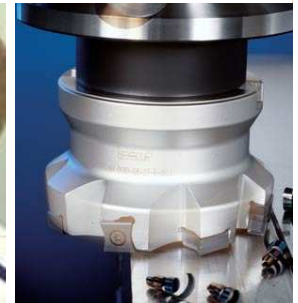
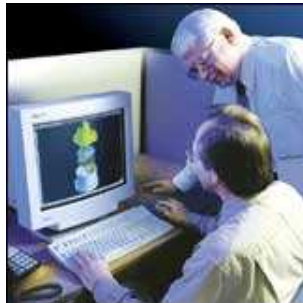


Manufacturing Engineering 2

BAGGT23NEC

2013/14 I.


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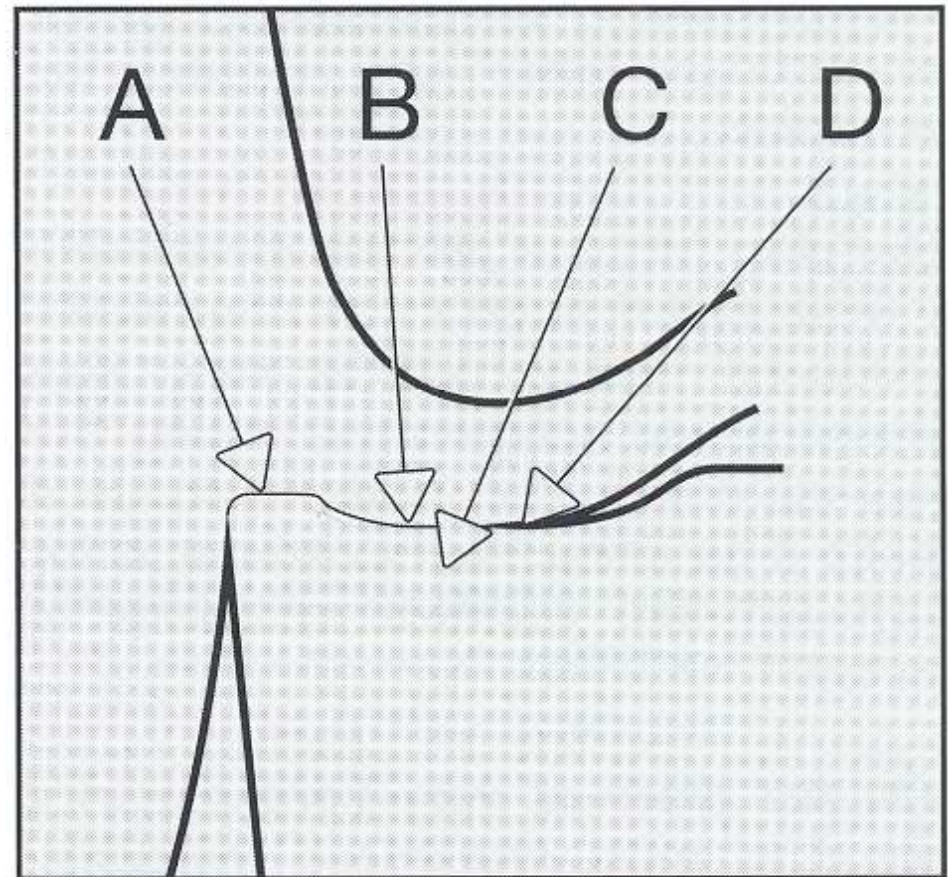


CUTTING PERFORMANCES

- 
- **Tool wear**
 - Load of a cutting tool
 - Tool wear mechanisms
 - Tool wear types
 - **Forces**
 - **Cooling**

Load factors of a tool

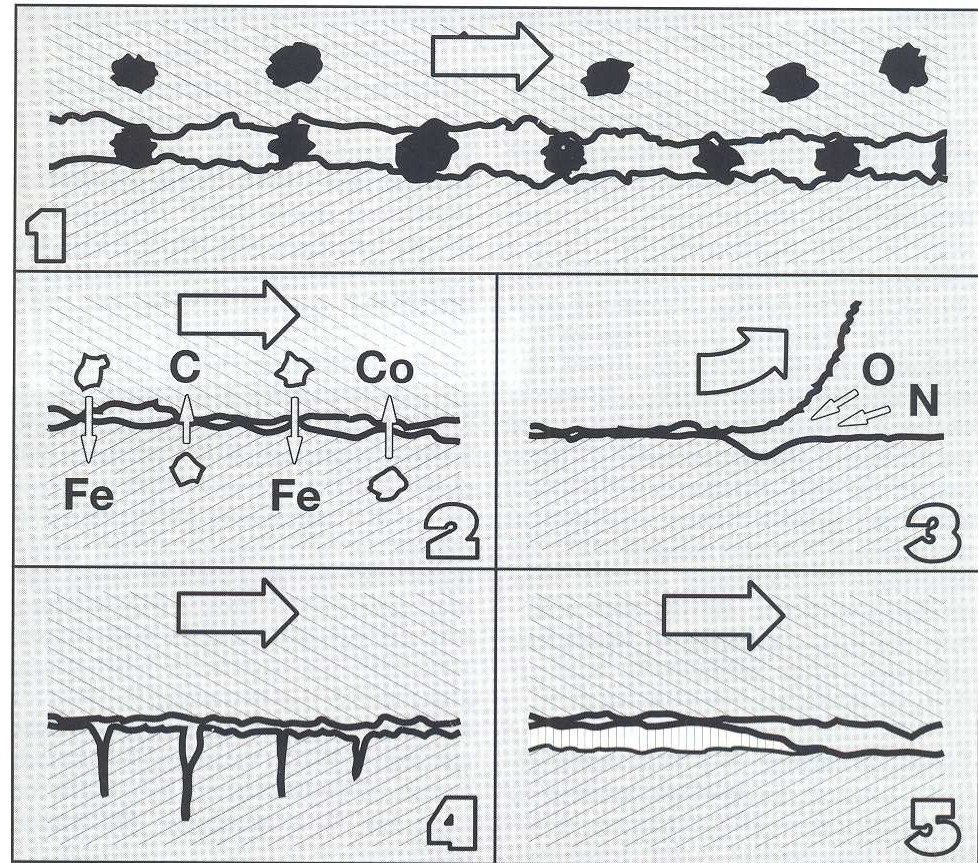
- A – mechanical
- B – thermal
- C – chemical
- D - abrasive



Typical wear zones

Tool wear mechanism

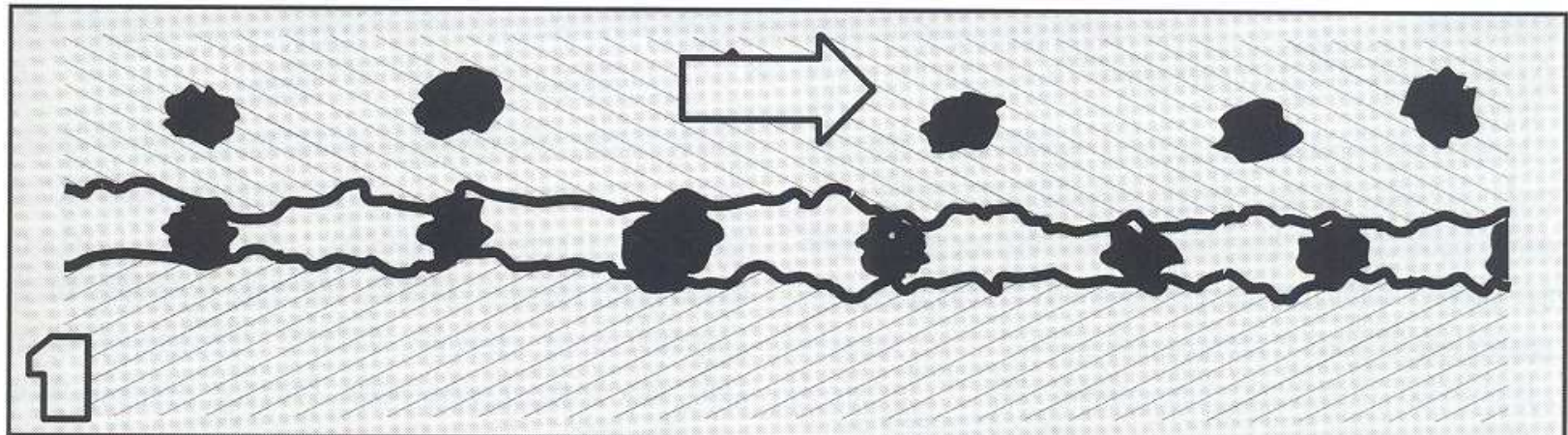
- 1 – abrasion wear
- 2 – diffusion wear
- 3 – oxidation wear
- 4 - fatigue wear
- 5 - adhesion wear



Basic wear mechanisms in metal cutting

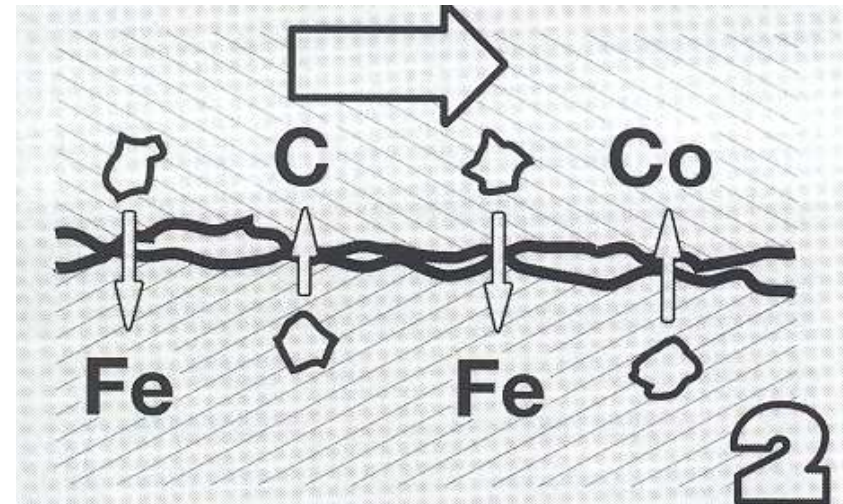
Abrasive wear

- Friction
- Different hardness
- Mechanical load



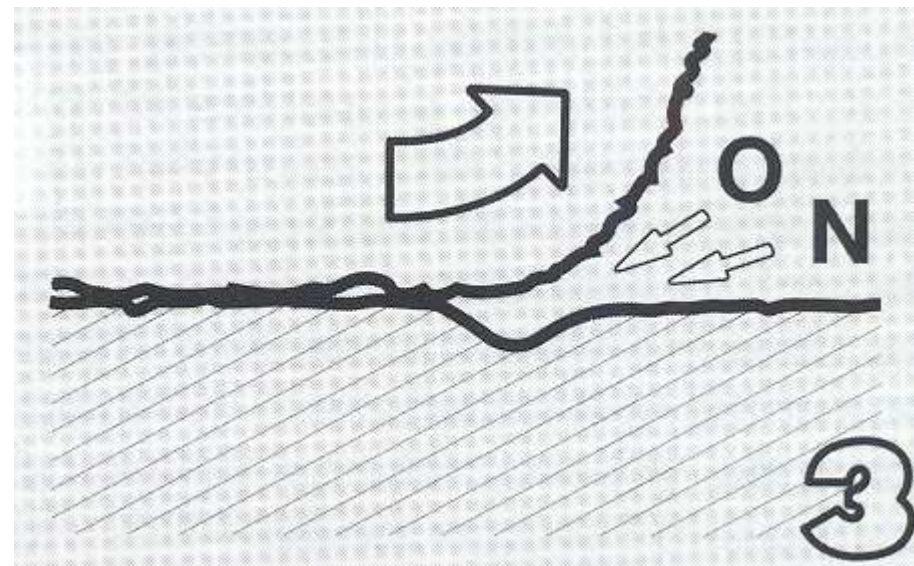
Diffusion wear

- Different chemical properties
- Atomic interchange
- Affinity of the tool material to the workpiece material
- Temperature depend
- High cutting speed



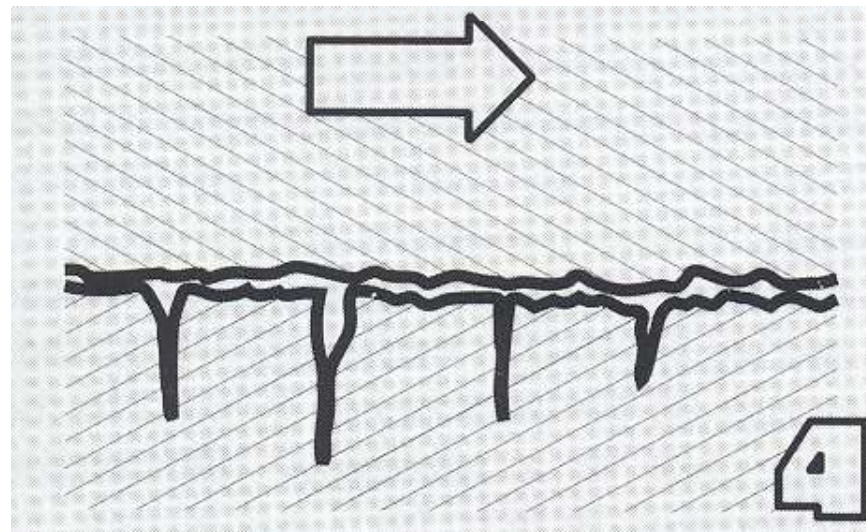
Oxidation wear

- High temperature + Air (oxygen)
- Some oxides are harder than the tool material



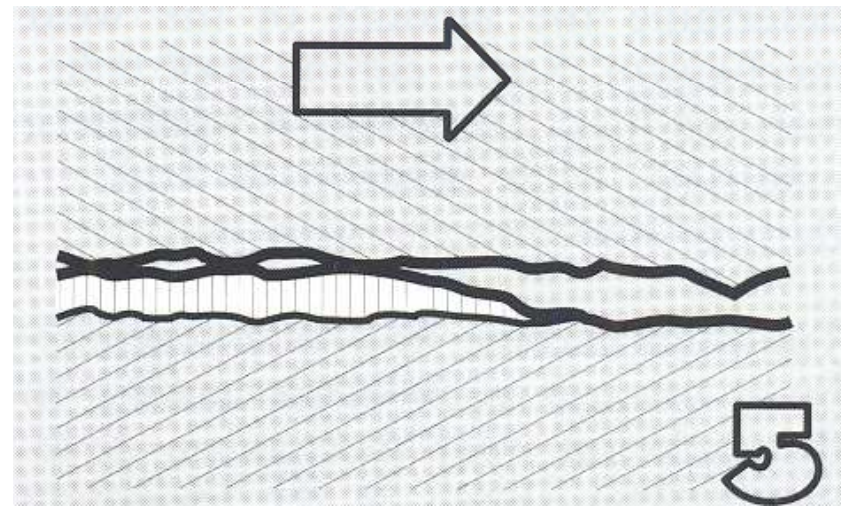
Fatigue wear

- Thermo-mechanical process
- Change of thermal and mechanical load
- Breaking

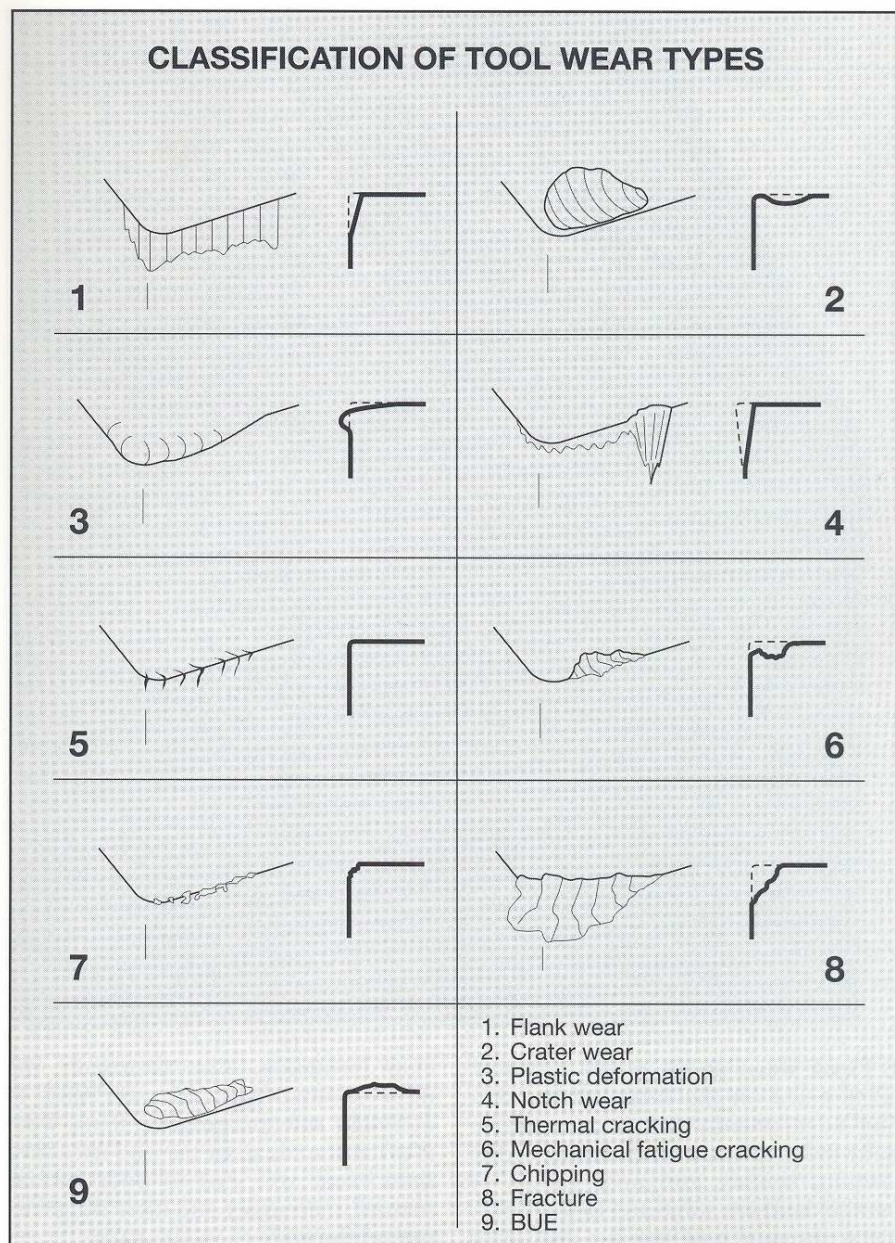


Adhesion wear

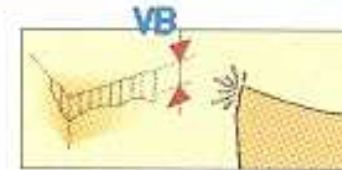
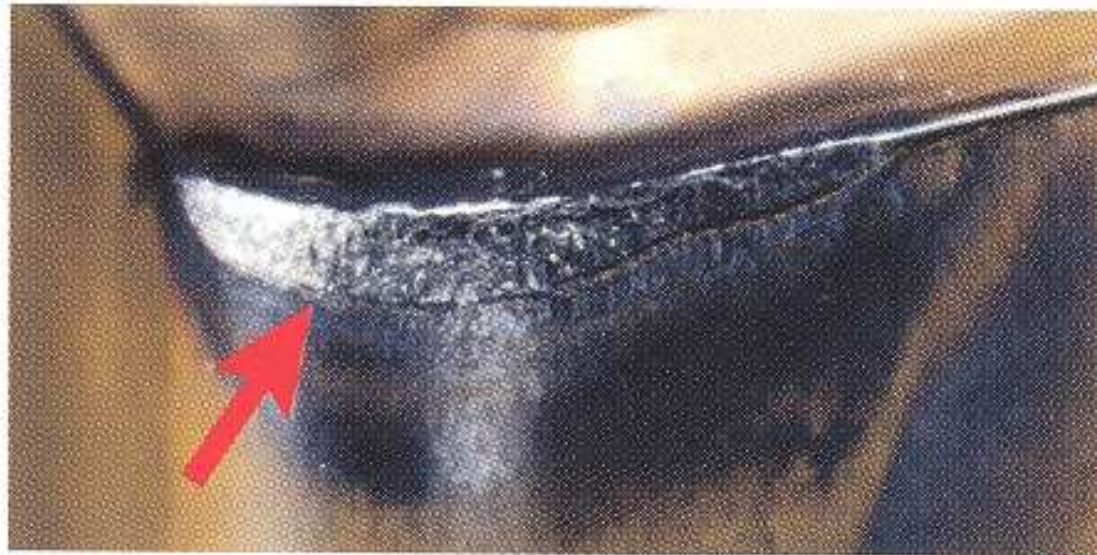
- Low machining temperature
- The chip is welded to the tool – build-up edge (BUE)



Tool wear types



Flank wear



FLANK WEAR

Tool wear

Rapid flank wear causing poor surface texture or inconsistency in tolerance.

Possible cause

Cutting speed too high or insufficient wear resistance.

Possible remedy

Select a more wear resistant grade.

For work-hardening materials, select a smaller entering angle.

Reduce cutting speed when machining heat resistant material.

Crater wear



CRATER WEAR

Tool wear

Excessive crater wear causing a weakened edge and poor surface finish.

Possible cause

Excessive cutting temperatures and pressure on the top face of inserts.

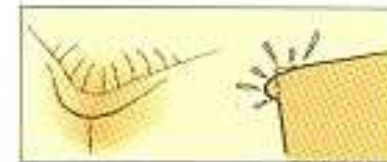
Possible remedy

First, reduce cutting speed to obtain a lower temperature and secondly, the feed.

Select a more wear resistant grade.

Select a positive insert geometry

Plastic deformation



PLASTIC DEFORMATION

Tool wear

Plastic deformation of edge, depression or flank impression, leading to poor chip control poor surface finish and insert breakage.

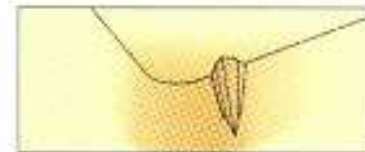
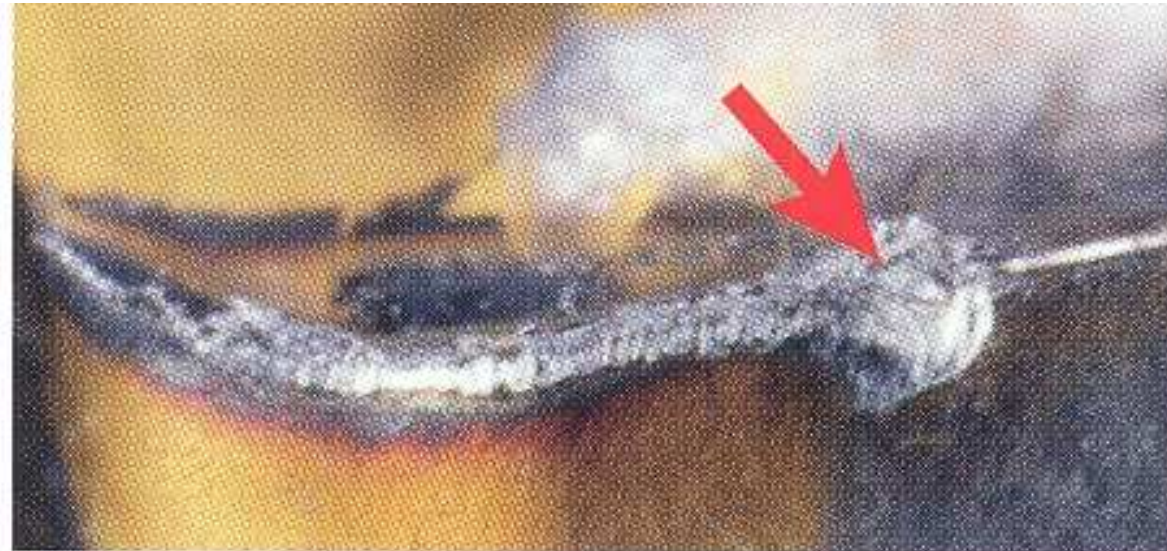
Possible cause

Cutting temperature and pressure too high.

Possible remedy

- Select a more wear resistant grade, which is harder.
- Reduce cutting speed.
- Reduce feed.

Notch wear



NOTCH WEAR

Tool wear

Notch wear causing poor surface texture and risk of edge breakage.

Possible cause

Cutting speed too high or insufficient wear resistance.

Possible remedy

Select a more wear resistant grade.

For work-hardening materials, select a smaller entering angle.

Reduce cutting speed when machining heat resistant material.

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Thermal cracking



THERMAL CRACKS



Tool wear

Small cracks perpendicular to the cutting edge causing chipping and poor surface finish.

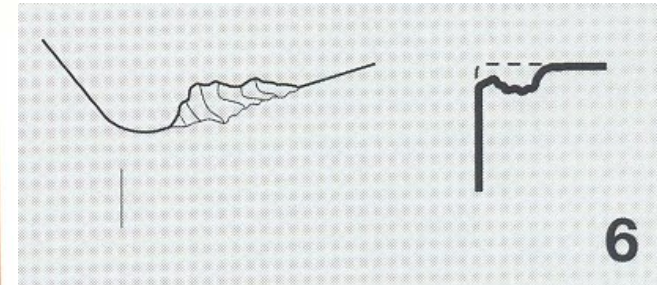
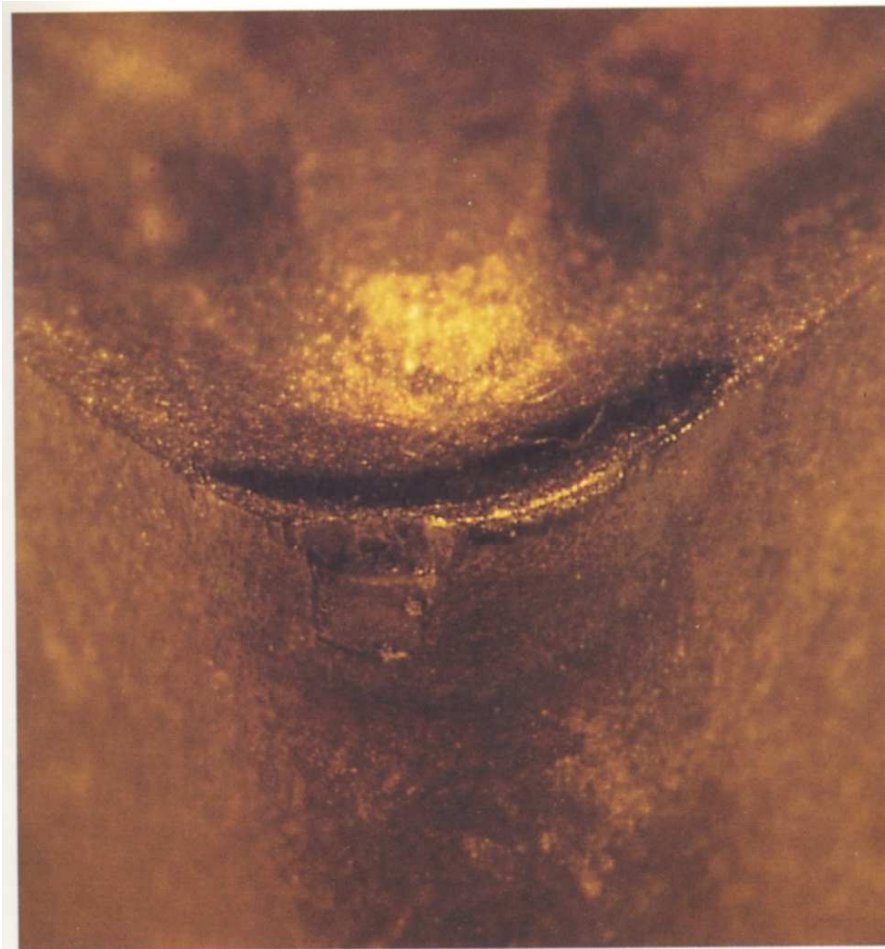
Possible cause

Excessive temperature variations.
Intermittent machining.
Varying coolant supply.

Possible remedy

Select a tougher insert grade.
Coolant should be applied copiously or not at all.

Mechanical fatigue cracking



6. Mechanical fatigue cracking can take place when the cutting force shocks are excessive. It is fracture due to continual variations in load where the load in itself is not large enough to cause fracture. Start of cut and variations in cutting force magnitude and direction may be too much for the strength and toughness of the insert.

These cracks are mainly parallel to the cutting edge.

Chipping of the edge



CHIPPING

Tool wear

Small cutting edge chipping leading to poor surface texture and excessive flank wear.

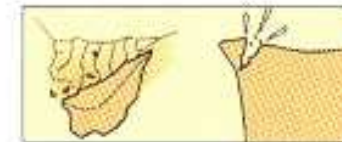
Possible cause

Cutting edge too brittle.
Insert edge too weak.
Built-up edge has been formed.

Possible remedy

Select tougher grade.
Select an insert with a stronger cutting edge.
Increase cutting speed. Select a positive geometry.
Reduce feed at beginning of cut.
Improve stability.

Fracture



EDGE FRACTURE

Tool wear

Damages not only the insert but can also ruin the shim and workpiece.

Possible cause

Excessive tool wear.
Grade and geometry too weak.

Excessive load on the insert.

Built-up edge has been formed.

Possible remedy

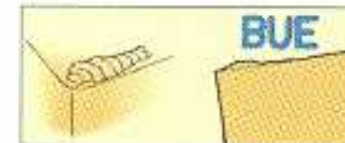
Reduce feed and/or depth of cut.

Select a stronger geometry, preferably a single sided insert.

Select a thicker/larger insert and tougher grade.

Improve stability.

Built-up edge (BUE)



BUILT-UP EDGE

Tool wear

Built-up edge causing poor surface finish and cutting edge chipping, when the BUE is torn away.

Possible cause

Cutting zone temperature is too low.

Negative cutting geometry.

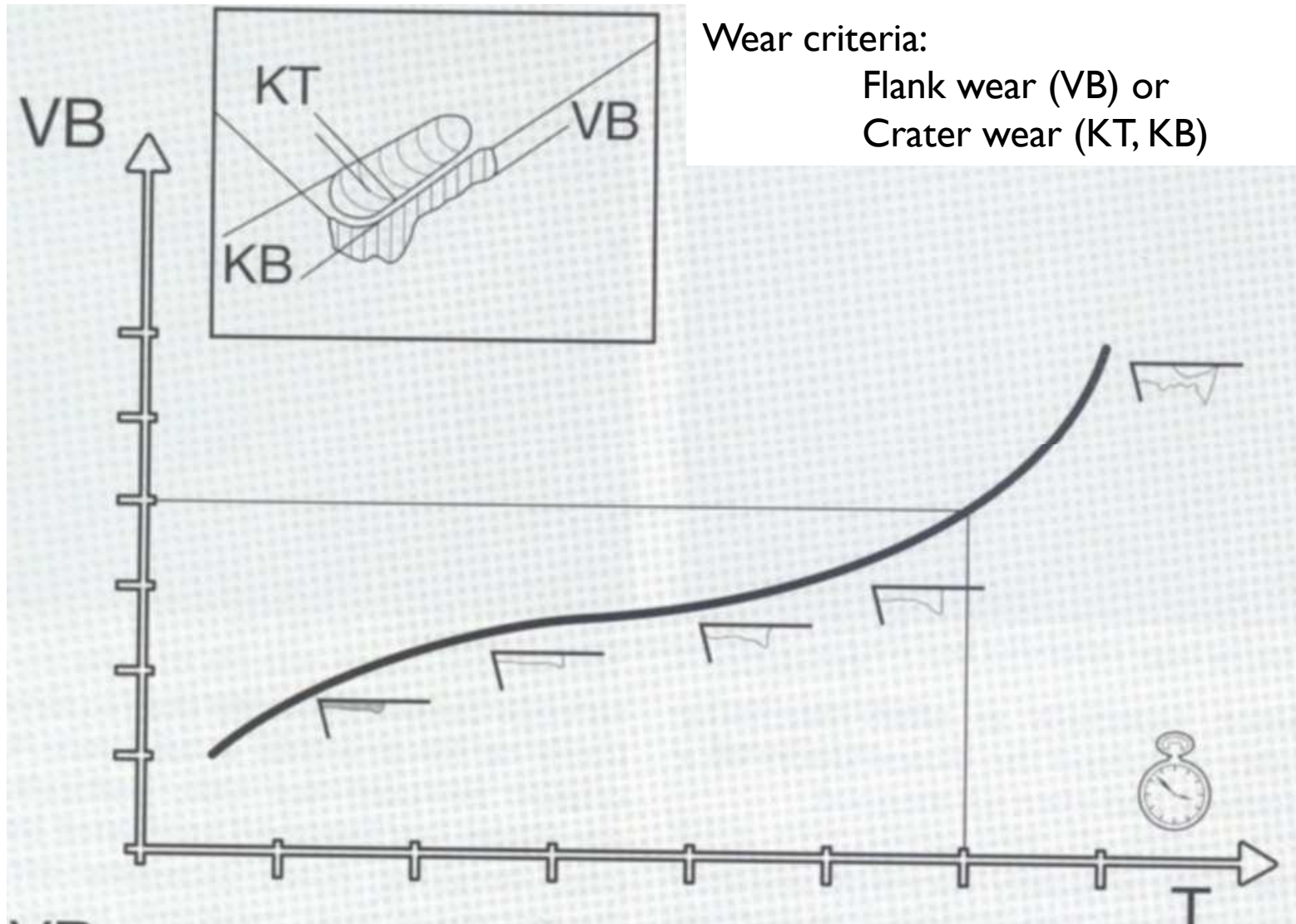
Very sticky material, such as low-carbon steel, stainless steels and aluminium.

Possible remedy

Increase cutting speed.
Change to a more suitable coated grade.

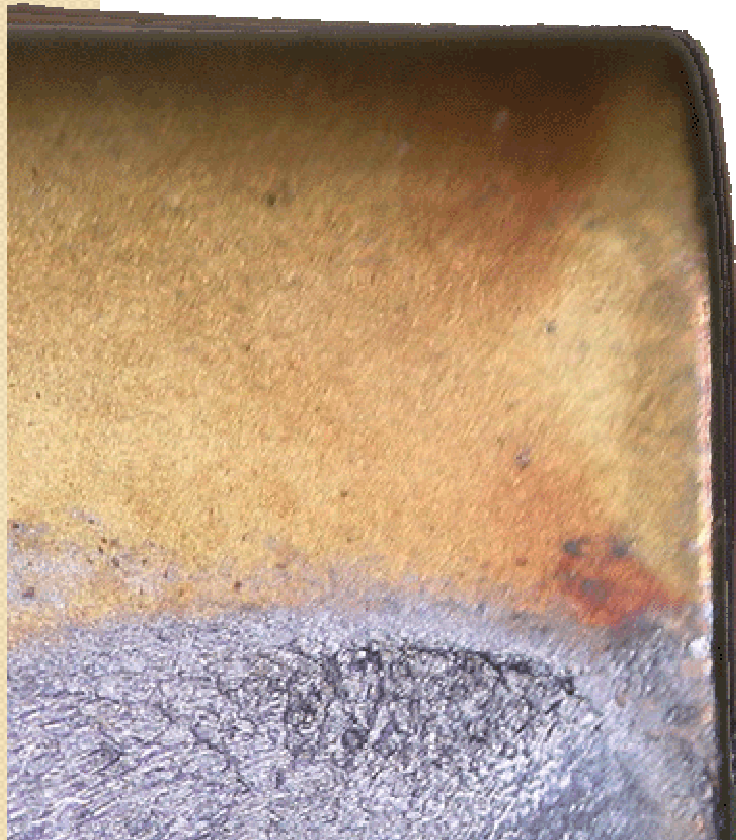
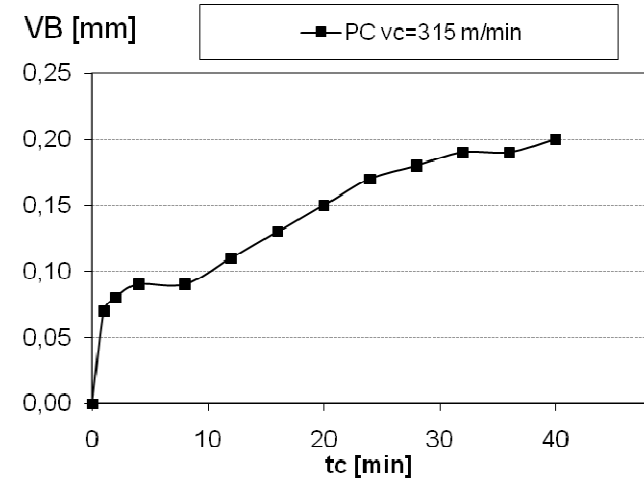
Select a positive geometry insert.

Wear process

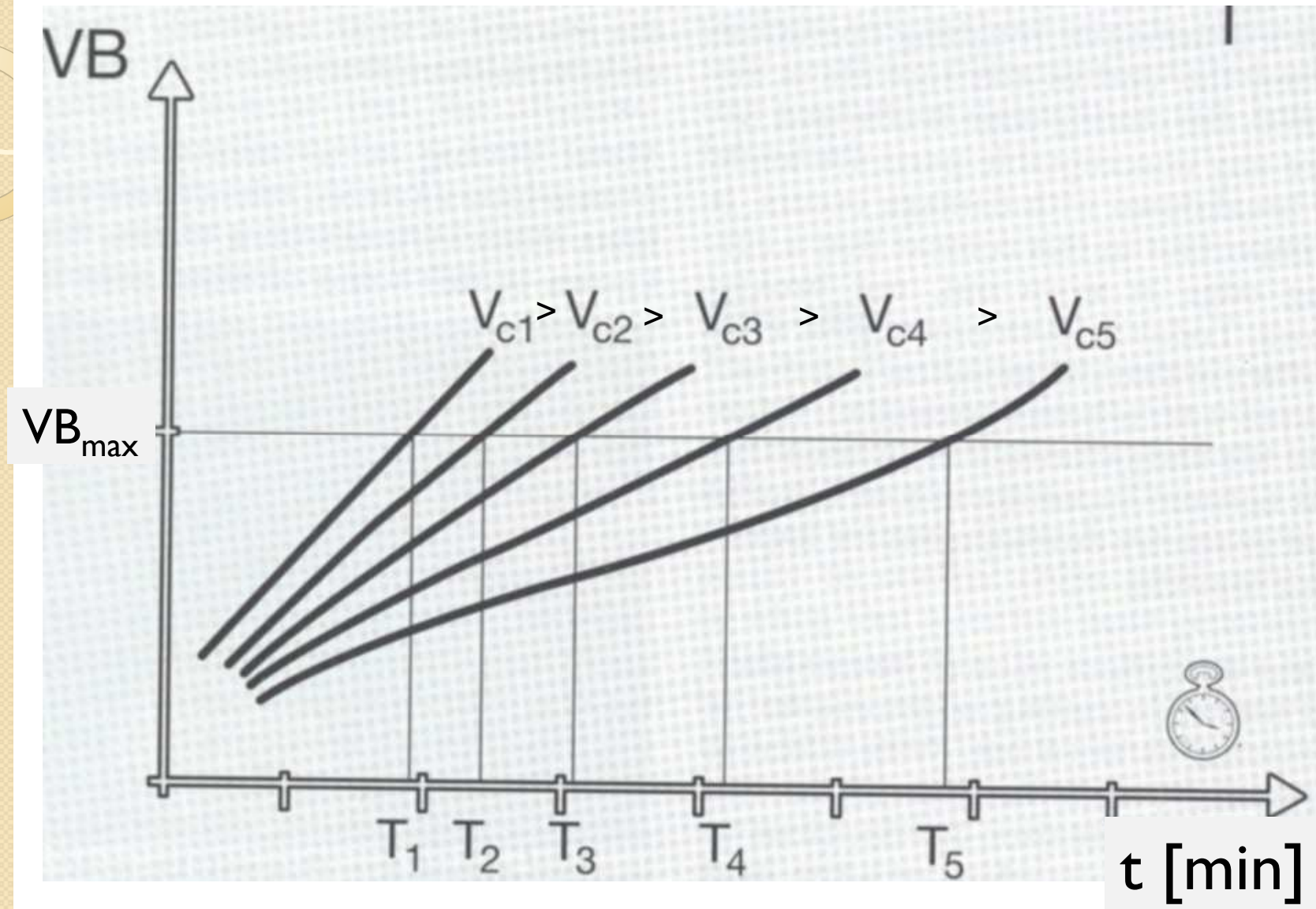


Wear process

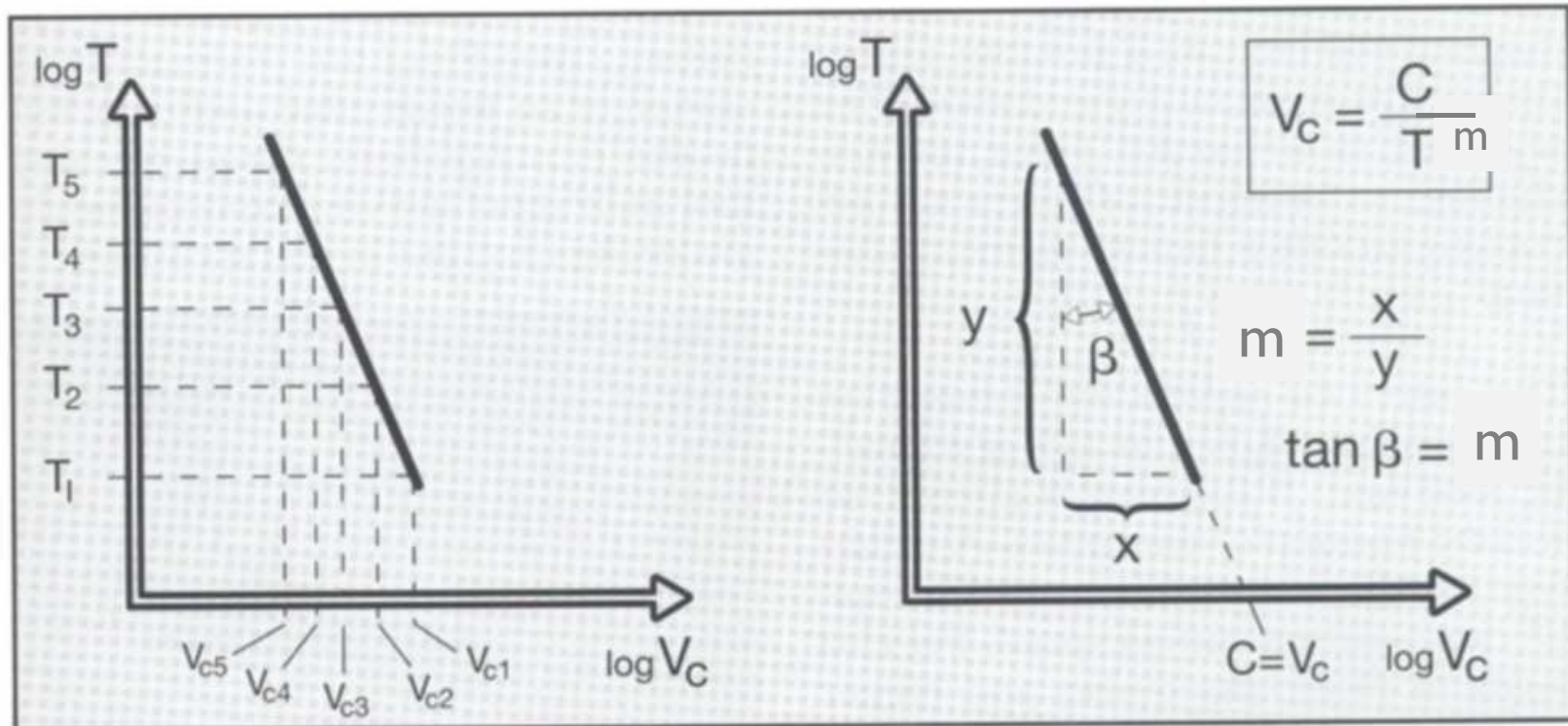
- Cutting speed: $v_c = 315$ m/min
- Depth of c.: $a = 1,5$ mm
- Feed: $f = 0.2$ mm
- Material: C45



Wear vs. Cutting speed



Logarithmic diagram



m – Constant, depends on workpiece material

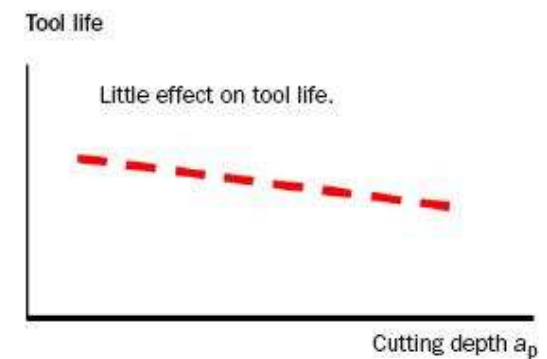
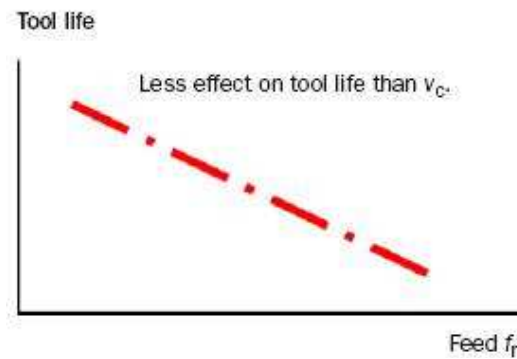
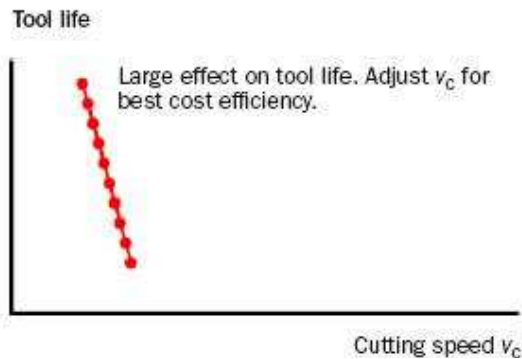
T – Tool life

1907. W. A. Taylor – turning, v_c

Extended Taylor formulae

Turning

$$v_c = \frac{C_v}{f^{x_v} \cdot a^{y_v} \cdot T^m} \left[\frac{\text{m}}{\text{min}} \right]$$



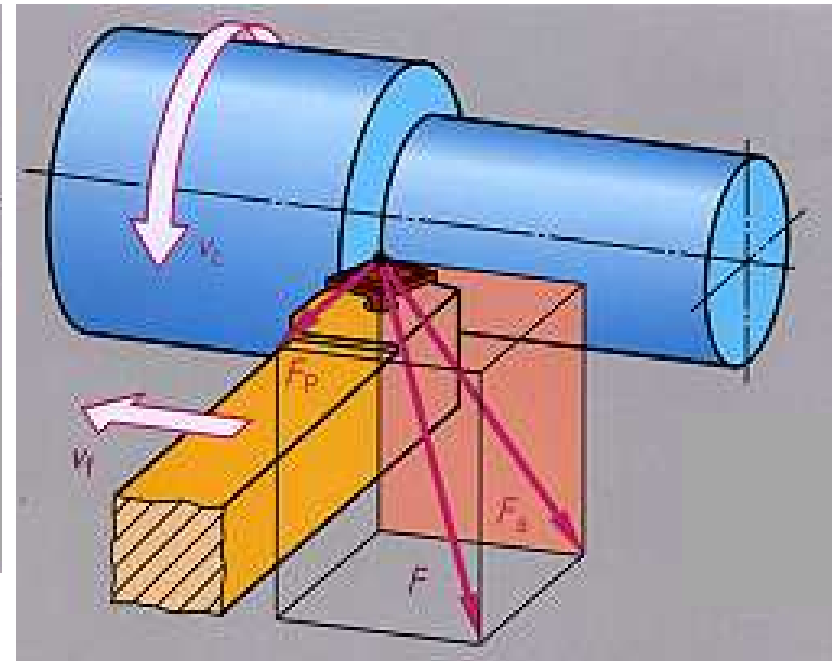
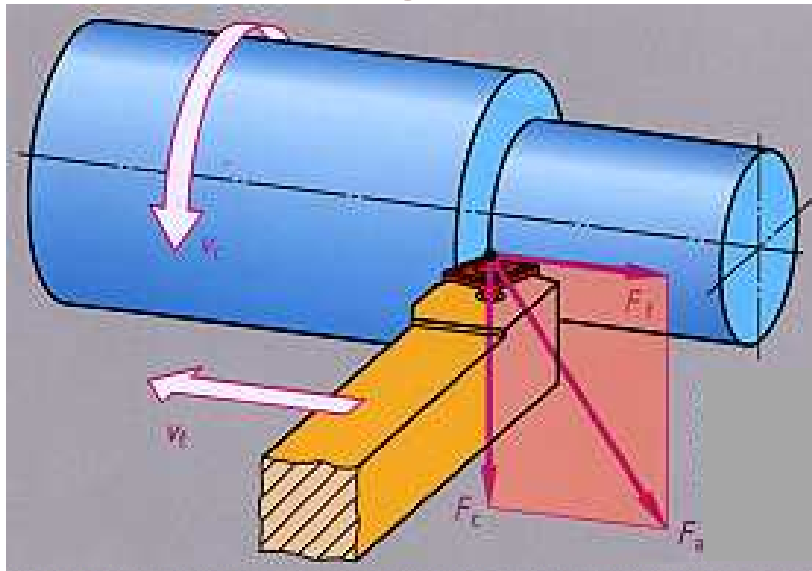
Drilling

$$v_c = \frac{C_v \cdot d^{z_v}}{f^{x_v} \cdot T^m} \left[\frac{\text{m}}{\text{min}} \right]$$

Milling

$$v_c = \frac{C_v}{f_z^{x_v} \cdot a_e^{y_v} \cdot a_p^{z_v} \cdot T^m} \left[\frac{\text{m}}{\text{min}} \right]$$

Cutting forces



F – Cutting force

F_c – Tangential component of the cutting force

F_f – Axial component of the cutting force (feed force)

F_a – Active cutting force

F_p – Radial component of the cutting force (pasive force)

Cutting force

Method 1 $F_c = k_c \cdot A \text{ [N]}$

$$k_c = \frac{k_{c1}}{h^m}$$

k_c – specific cutting force,

required force for cutting a 1 mm² chip

k_{c1} – main value of the specific cutting force

h – chip thickness

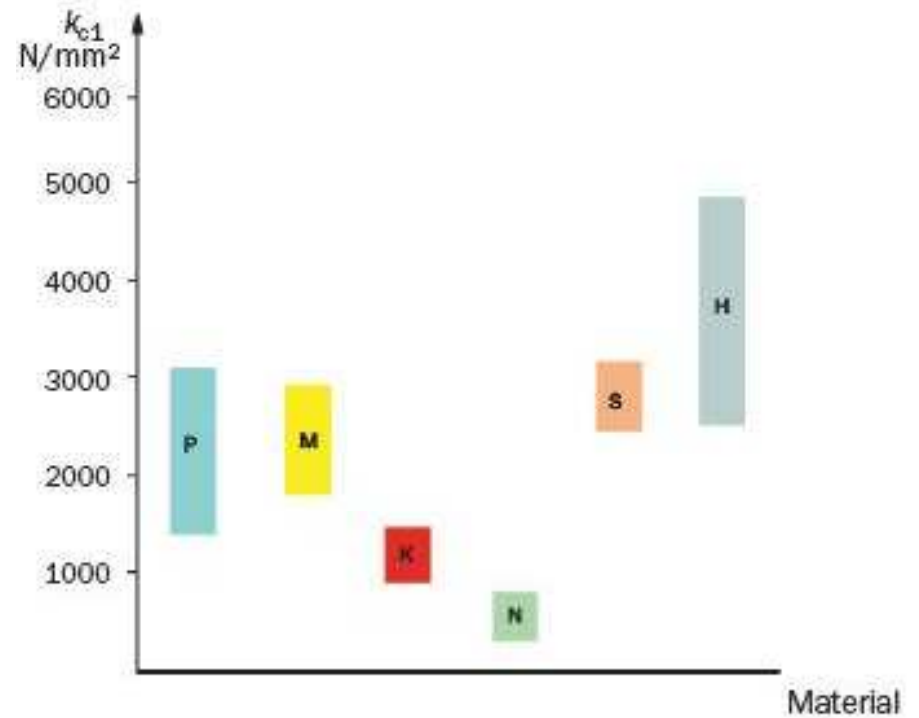
m - exponent

A – chip cross section area ($A = a f = b h$)

$$F_c : F_p : F_f = 100 : 40 \div 80 : 10 \div 30$$

$$F_p = A \cdot \frac{k_{p1}}{h^m} \text{ [N]} \quad F_f = A \cdot \frac{k_{f1}}{h^m} \text{ [N]}$$

Material	k_{c1}	m
C15	1820	0,22
C45	1680	0,26
100Cr6	1410	0,39
90MnCrV	2300	0,21
x5CrNi1810	2350	0,21
GG20	1020	0,25
AlMg3	780	0,23



Method 2

$$F_c = C_F \cdot f^{x_F} \cdot a^{y_F} \cdot v_c^{z_F} \cdot \prod K_{Fci} \quad [\text{N}]$$

C_F – constant coefficient, N

x_F , y_F , z_F - exponent

a , f , v_c – cutting data

K_{Fci} – modification coefficients

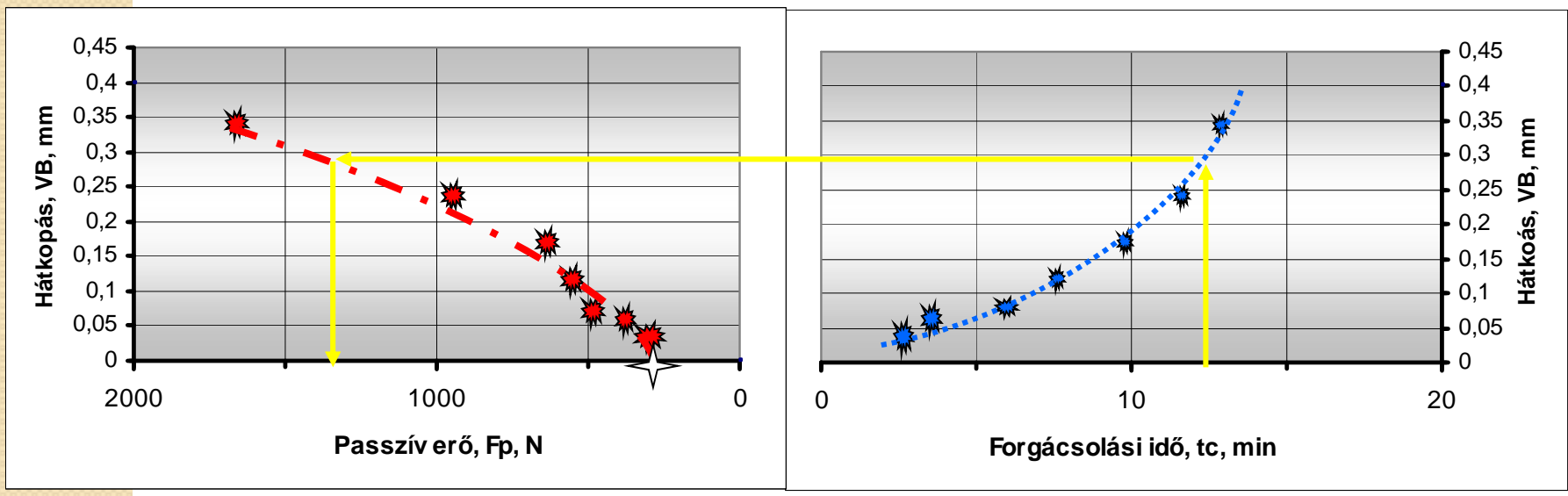


Torque in the axes, Nm

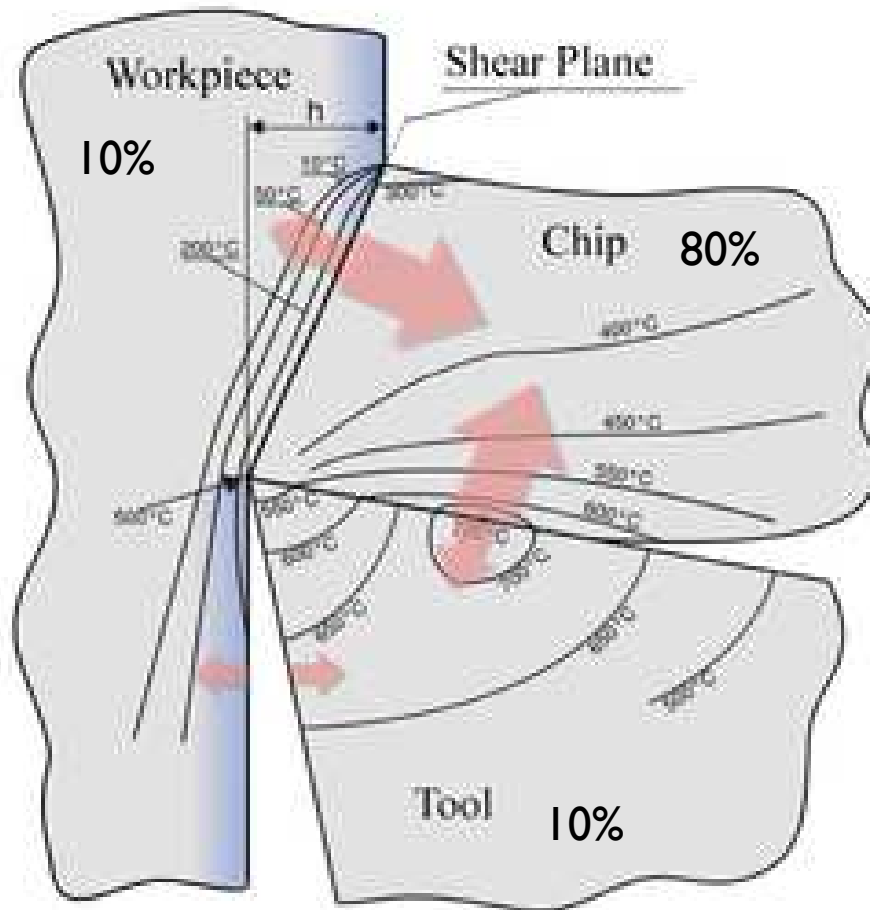
$$M_c = \frac{F_c \cdot d}{2000} \quad [\text{Nm}]$$

Power, kW

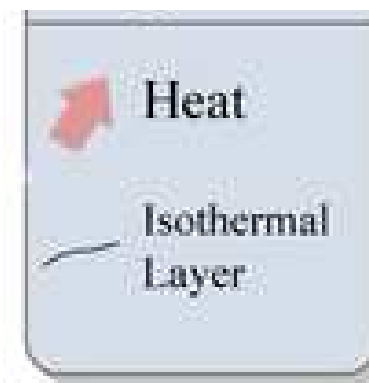
$$P_c = \frac{F_c \cdot v_c}{60000} = \frac{M_c \cdot n}{9550} \quad [\text{kW}]$$



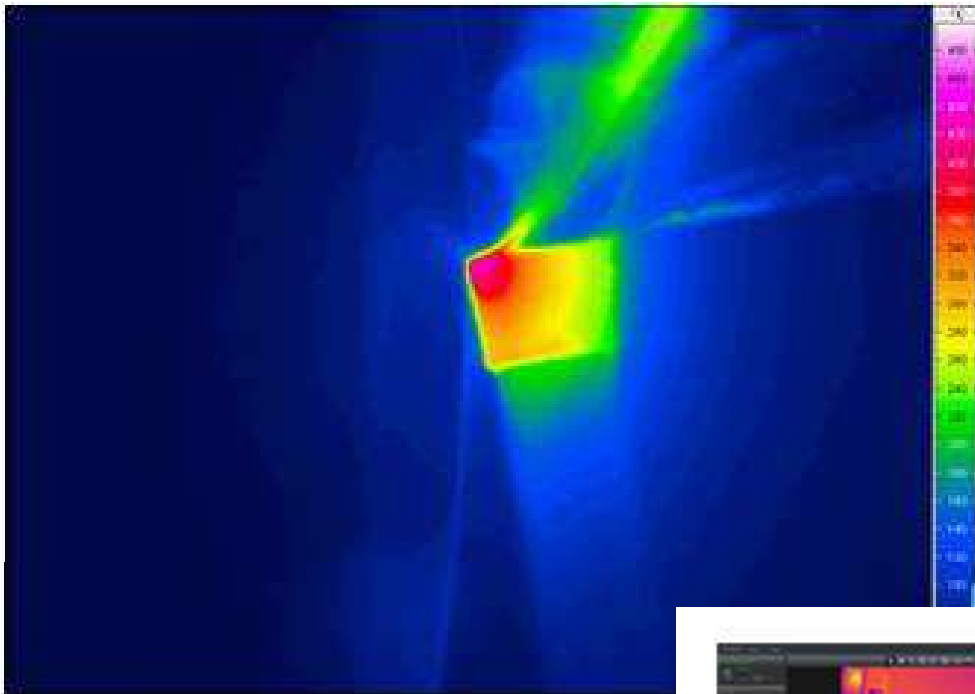
Temperature



- Shearing
- Friction
- Load (cutting force)



Measure?



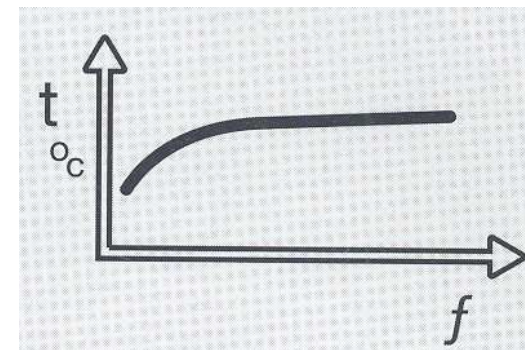
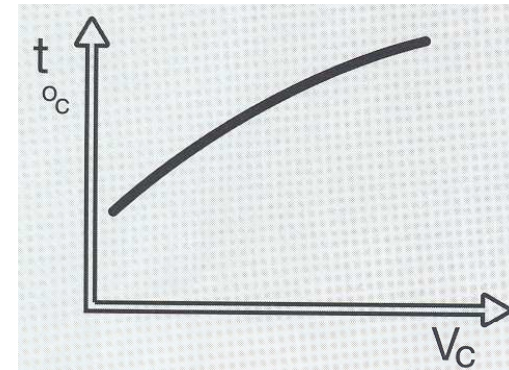
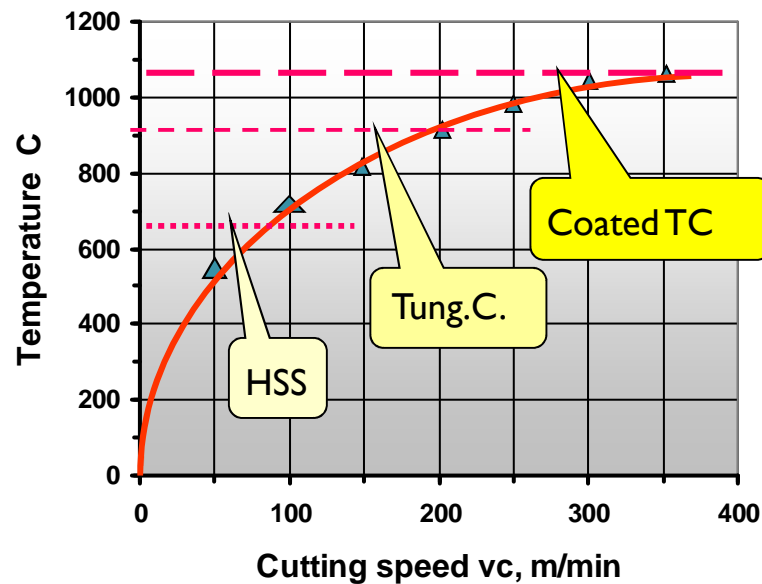
Calculation

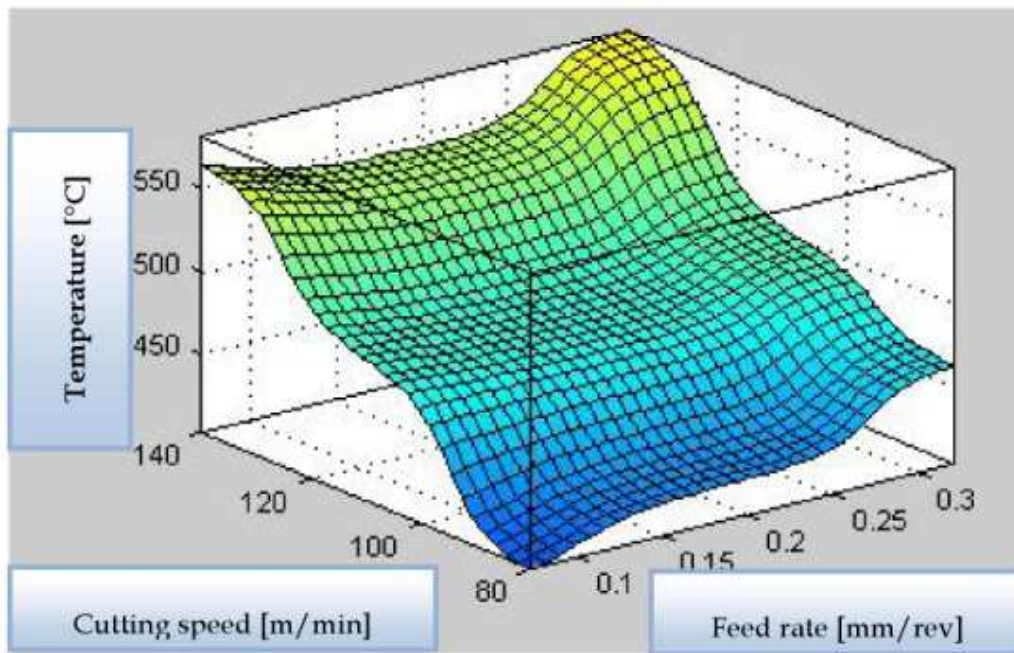
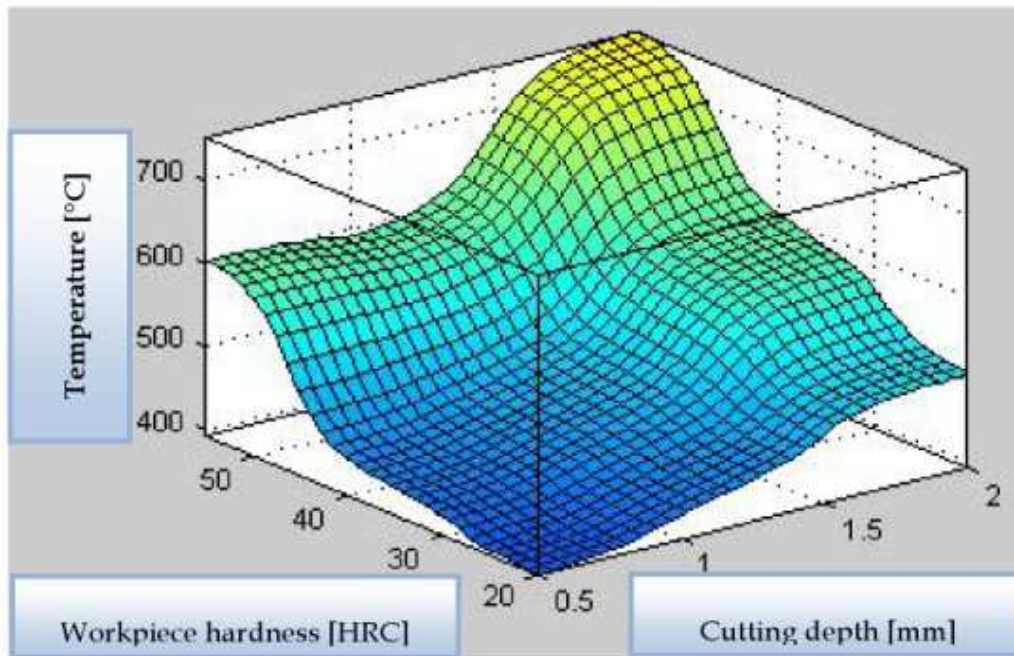
$$\Theta = C_{\Theta} \cdot f^{x_{\Theta}} \cdot a^{y_{\Theta}} \cdot v_c^{z_{\Theta}} \text{ [}^{\circ}\text{C]}$$

C_{Θ} – constant coefficient

$x_{\Theta}, y_{\Theta}, z_{\Theta}$ – exponent (<1)

a, f, v_c – cutting data





Coolant

- Aim / function:
 - Cooling - detract the heat
 - Lubricating - decrease the friction
 - Flushing - wash-out the chips

Coolant material

- Non (dry cutting)
- Air (C, F)
- Cool air (C, F)
- Oil (L)
- Water + oil (C, L, F)

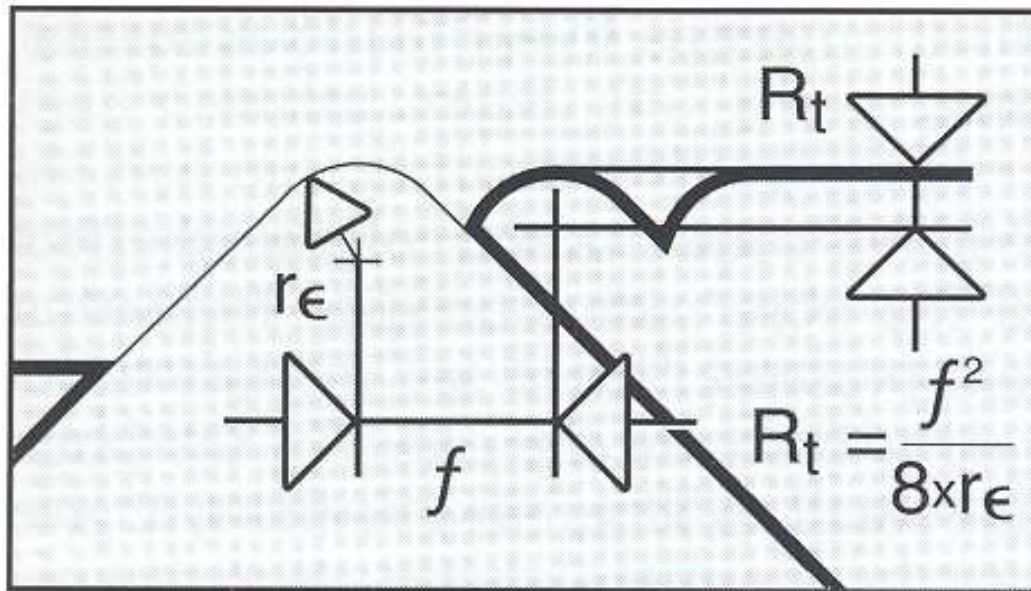




Surface quality

- Accuracy
 - Size
 - Shape
 - Position
- Surface quality
 - Surface roughness
 - Surface integrity

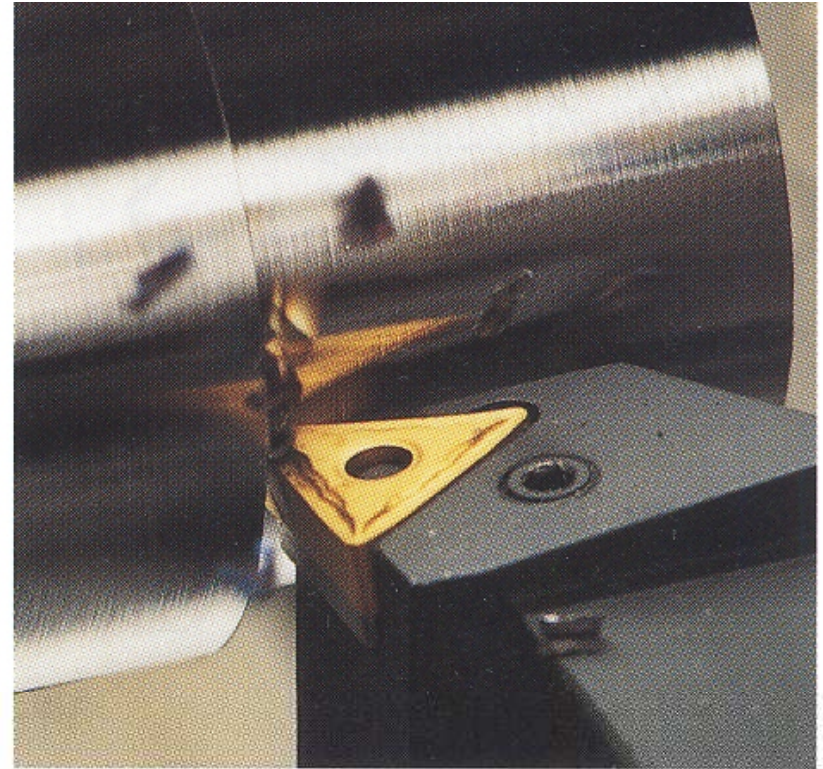
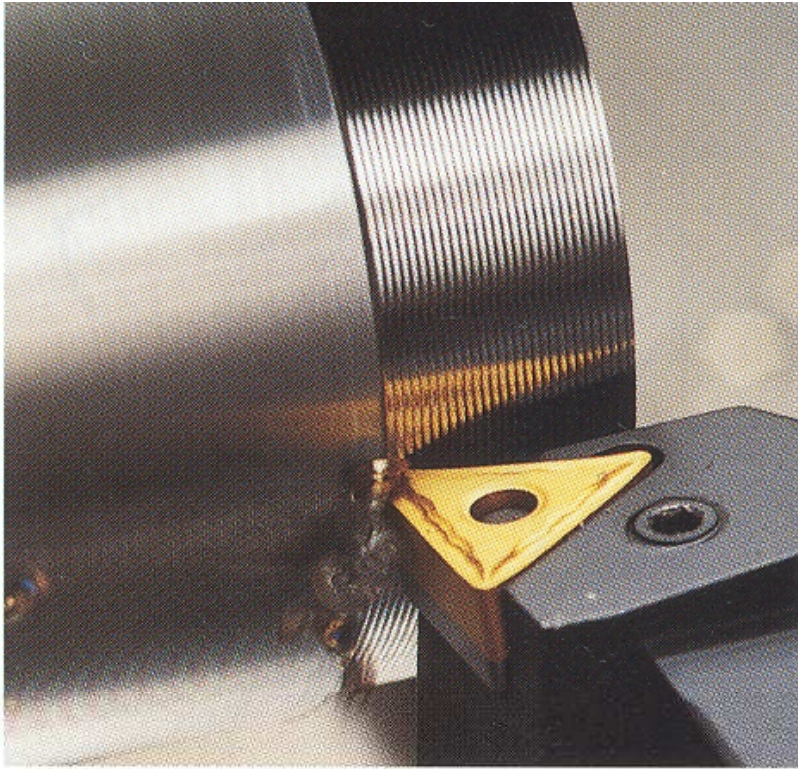
Surface roughness in turning



Main factors:

- Feed
- Nose radius

$$R_t \approx 4 R_a$$



The nose radius affects surface texture and cutting edge strength